

Interpretation of the transpulmonary pressure in the critically ill patient

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Abstract: Mechanical ventilation is a life-saving procedure, which takes over the function of the respiratory muscles while buying time for healing to take place. However, it can also promote or worsen lung injury, so that careful monitoring of respiratory mechanics is suggested to titrate the level of support and avoid injurious pressures and volumes to develop. Standard monitoring includes flow, volume and airway pressure (Paw). However, Paw represents the pressure acting on the respiratory system as a whole, and does not allow to differentiate the part of pressure that is spent to distend the chest wall. Moreover, if spontaneous breathing efforts are allowed, the Paw is the sum of that applied by the ventilator and that generated by the patient. As a consequence, monitoring of Paw has significant shortcomings. Assessment of esophageal pressure (Pes), as a surrogate for pleural pressure (Ppl), may allow the clinicians to discriminate between the elastic behaviour of the lung and the chest wall, and to calculate the degree of spontaneous respiratory effort. In the present review, the characteristics and limitations of airway and transpulmonary pressure monitoring will be presented; we will highlight the different assumptions underlying the various methods for measuring transpulmonary pressure (i.e., the elastance-derived and the release-derived method, and the direct measurement), as well as the potential application of transpulmonary pressure assessment during both controlled and spontaneous/assisted mechanical ventilation in critically ill patients.

Keywords: Esophageal pressure (Pes); transpulmonary pressure; mechanical ventilation; critically ill patients

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Introduction: mechanical ventilation and ventilator-induced lung injury (VILI)

As a part of the supportive therapy of modern intensive care medicine, the majority of critically ill patients undergo invasive mechanical ventilation during their stay in the intensive care unit. However, mechanical ventilation does support the function of the lungs; instead, from a pathophysiological point of view, it is a substitute for the activity of respiratory muscles, which is undertaken to buy time for healing to take place (1).

Of note, soon after its introduction into modern critical care (2), it was discovered how mechanical ventilation itself could lead to a structural damage to the lung (3). Indeed, a completely “safe” form of mechanical ventilation has not been found yet, as the main side-effects associated with this technique are the hemodynamic instability due to the increased intrathoracic pressures, and the direct mechanical trauma to the structure of the lungs. In fact, it has repeatedly been shown how mechanical ventilation itself can lead to worsening injury of previously damaged lungs, or it can damage the lungs even in the absence of a pre-

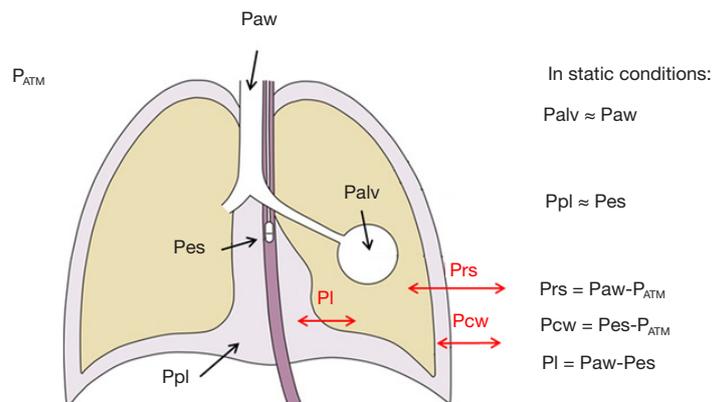


Figure 1 Model of the respiratory system, as composed by the lungs and the chest wall in series. The figure shows the different pressure within the system and the relative distending forces (in red). P_{ATM} , atmospheric pressure; P_{aw} , airway pressure; P_{es} , esophageal pressure; P_{alv} , alveolar pressure; P_{pl} , pleural pressure; P_{rs} , transrespiratory pressure; P_{cw} , trans-chest wall pressure; P_l , transpulmonary pressure.

existing lung injury. This injury has collectively been termed VILI (4). Two main mechanisms may injure the lung: firstly, excessively high inspiratory pressures and volumes (respectively identified by lung stress and strain), leading to an excessive distention of the alveolar wall, may cause injurious stretching/overdistention in the lung parenchyma (4,5). On the other side, VILI may occur when the airway pressure (P_{aw}) and expiratory volume are too low, as a consequence of inadequate positive end-expiratory pressure (PEEP) levels, as this may cause cyclic alveolar recruitment/derecruitment with each breath and an excessive tension at margins between aerated/nonaerated lung regions.

In an attempt to reduce the iatrogenic load secondary to the delivery of mechanical ventilation, extensive research has been conducted to identify less injurious ventilator strategies (6). The so-called “protective ventilation” is a paradigm that aims to an individual tailoring of ventilatory support. The current mainstay of such an approach are a low tidal volume ventilation, and the avoidance of elevated P_{aws} . Indeed, even with such an approach, it was shown how a significant proportion of critically ill patients may experience some degree of tidal hyperinflation (7), highlighting our still incomplete understanding of the pathophysiology of VILI.

Indeed, while alveolar pressure is relatively easy to estimate clinically as the P_{aw} during a period of zero flow (either during an expiratory, or an inspiratory hold manoeuvre), it only represents the pressure that is distending the respiratory system. Since the lungs and the chest wall are two elastic structures in series, a fraction of ventilator-delivered pressure is dissipated in

inflating the chest wall rather than the lung (*Figure 1*). Measuring the pressure that distends the lungs only, i.e., the transpulmonary pressure, may then be a better approach to guide ventilator management.

Moreover, as during assisted modes of breathing the patient inspiratory muscles share part of the total work of breathing (WOB) with the mechanical ventilator, so that the pressure which inflates the lungs is the sum of that applied by the ventilator and that applied by the patient, the only way to directly assess the patient contribution to the assisted breath is to measure its muscle pressure, i.e., the negative pleural pressure (P_{pl}) generated by its inspiratory muscles.

The present review examines the characteristics and limitations of the monitoring of airway and transpulmonary pressure, and it highlights the potential application of transpulmonary pressure assessment during both controlled and spontaneous/assisted mechanical ventilation in critically ill patients.

Limits of P_{aw} monitoring

Ever since the early applications of invasive mechanical ventilation as a form of respiratory support for critically ill patients, pressure-based respiratory mechanics have guided the clinicians when adjusting the ventilator (8). However, measurements based only on P_{aw} may not be easily generalized in a patient population with different pathologic conditions. In fact, the main focus of the physician is the mechanical behavior of the passive lungs, while P_{aw} -based interpretations of respiratory mechanics are often influenced

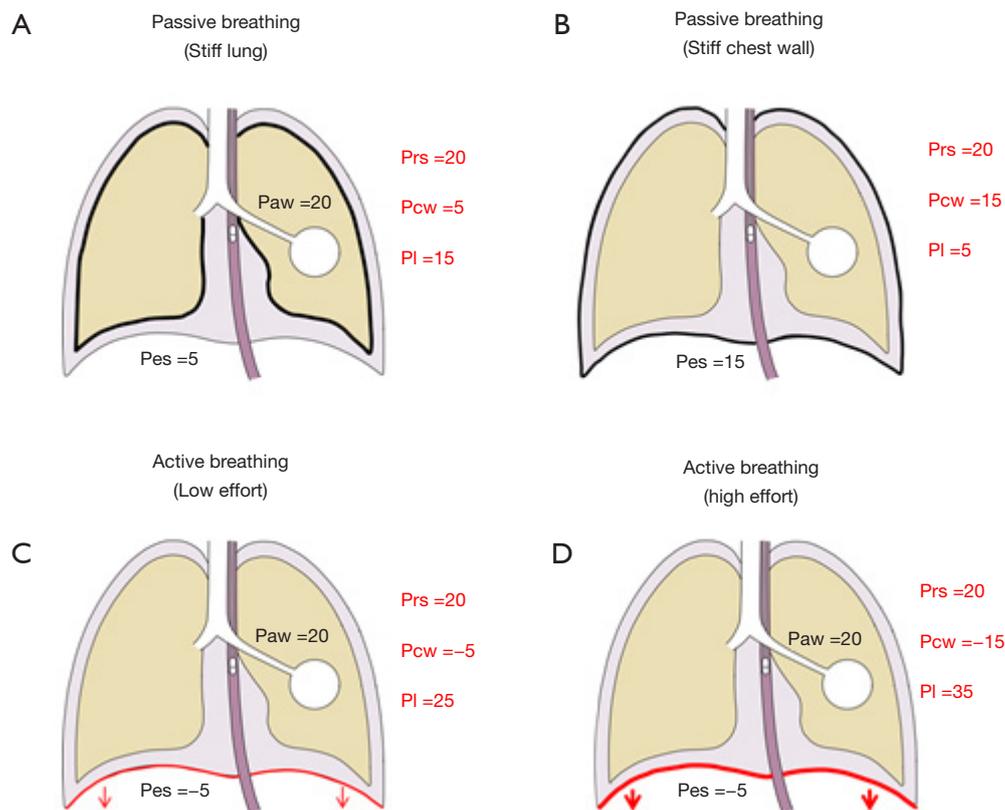


Figure 2 Utility of esophageal pressure measurement in both passive breathing during controlled mechanical ventilation (upper panel) and spontaneous breathing during assisted ventilation (lower panel). The upper panel shows the effect of different lung and chest wall mechanical properties on the pressure that actually distends the lung, i.e., the transpulmonary pressure, for the same given airway pressure. In (A), a “stiff” lung (i.e., one with a high elastance) is depicted, whereas in (B) the mechanical properties of the lung are normal, but this is coupled to a “stiff” chest wall. For the same airway pressure, in (A) the transpulmonary pressure is high, while in (B) it is low. The lower panel shows the effect of different levels of patient inspiratory effort on the transpulmonary pressure, for the same given airway pressure. In (C) a low level of effort is generated by the patient’s muscles, with acceptable levels of transpulmonary pressure; in (D) a high level of effort is present, which leads to the generation of an injuriously high transpulmonary pressure, despite similar values of airway pressure. Paw, airway pressure; Pes, esophageal pressure; Prs, transrespiratory pressure; Pcw, trans-chest wall pressure; Pl, transpulmonary pressure.

by several pathophysiological alterations: differences in breathing pattern, altered chest wall characteristics (often secondary to fluid overload) (9), alterations in lung volume, increased intra-abdominal pressure (IAP) (such as with capillary leak or fluid overload) (10), the extent of lung edema and collapse, the distribution and asymmetry of lung disease (11), the presence and extent of spontaneous breathing efforts (12). It has been shown how all of these factors do complicate the interpretation of respiratory mechanics, thus preventing the interpretation of Paw to be easily generalizable (13).

Setting the ventilator based on Paw measurements may indeed be adequate for most critically ill patients. However,

Paw is an oversimplified surrogate for the pressure in the lungs, as the respiratory system is composed of two elastic structures in series, namely the chest wall and the lungs. Indeed, chest wall alterations are common in critically ill patients, and they may not be easily predicted (10,14-17); as a consequence, the contribution of the chest wall to respiratory system mechanics should not be ignored. For each tidal volume, a stiffer chest wall implies the development of higher Ppl, as a greater part of the driving pressure is spent to move the chest wall. As a consequence, the same Paw may lead to dramatically different transpulmonary Ppl depending on the chest wall properties, as exemplified in *Figure 2*, upper panel. Indeed, the pressure

shown on the ventilator display is in fact the P_{aw} , and in the clinical setting, this is the variable more commonly used to assess lung overdistention. However, correct interpretation of this variable requires knowledge of its determinants.

Although the use of low tidal volumes and limited plateau pressures are the current standard of care, this lung protective approach has been shown to provide an inadequate substitute when aiming to assess lung stress and strain, and the suggested limits may not be safe for all patients, depending on their relative characteristics of the chest wall (18,19). To this extent, Chiumello *et al.* demonstrated how, both in a group of patients with different severity of lung injury and in control medical and surgical patients undergoing mechanical ventilation for conditions different from respiratory failure, the ratio between lung and chest wall elastance (E_{cw}) may range from as low as 0.2 to as high as 0.8, making the interpretation of P_{aw} potentially misleading when extrapolating this data to estimate the pressure distending the lungs (P_l) (18).

In conclusion, the conventional management of ventilation based on P_{aw} -monitoring limits the chances to tailor the ventilator setting at the individual level. Individualized settings of mechanical ventilation may be the only way to provide effective and safe ventilation in more complex patients; to do so, the understanding of the overall influence of all these factors on respiratory system mechanics is of crucial importance.

In recent years, a renewed interest started to raise around the assessment of transpulmonary pressure (P_l , i.e., the pressure distending the lung), and this variable has increasingly been recommended to guide mechanical ventilation and to tailor it at the individual level. This physiologically sound, yet simple bedside tool may help clinicians to improve lung mechanics and gas exchange while at the same time avoiding lung injury in the more complex critically ill patients (20). In the following paragraphs, we will focus on the physiological rationale, measurement techniques and conditions that may influence esophageal pressure (P_{es}) monitoring, and on the potential clinical applications of transpulmonary pressure monitoring.

Pes monitoring: perks and pitfalls

As we said earlier, prediction of lung mechanical properties from P_{aw} measurements is often misleading, more so when the disease is unevenly distributed or spontaneous breathing efforts are allowed. Indeed, for a given P_{aw} , the portion of the applied pressure which is in fact applied to inflate only

the lungs could vary widely, depending on the mechanical characteristics of the chest wall (16). In this context, assessment of P_{pl} may be helpful to differentiate between patients who may benefit from a higher P_{aws} because of their increased chest wall elastance (E_{cw}) from those who, despite relatively low levels of P_{aw} , are still at risk of overdistention.

P_{pl} can experimentally be measured by inserting a device directly into the pleural space (21). However, this technique is invasive and it has never been used in the clinical practice. Moreover, direct introduction of a probe into the pleural space may potentially alter the mechanical characteristic of that space.

In the clinical ground, the conventional estimate of P_{pl} requires the measurement of P_{es} with a balloon-tipped catheter, a technique extensively used ever since the fifties for the physiological investigations of respiratory mechanics. Briefly, P_{es} is considered to be representative of the average value of P_{pl} surrounding the lungs, although this assumption is largely based upon studies in healthy subjects in the upright position (22-25). This assumption is based on the anatomical proximity of the lower third of the esophagus to the pleural space and the transmission of P_{pl} through its wall, as it mainly acts as a passive membrane.

As appealing as this approach seems to be, only in recent years, evidence for its effectiveness is beginning to be found. However, several authors raised concerns about the accuracy of P_{es} measurements in supine patients with altered lung function (that is, in different conditions from the “classic” respiratory physiology experiments) (26), and the significance of P_{es} as a proxy for the relevant P_{pl} .

In fact, several potential confounders may alter the estimation of P_{pl} from P_{es} , as summarized in *Table 1*. The pressure in the esophageal balloon may be influenced by the elastic recoil of the balloon itself, the elastic recoil of the esophagus and esophageal muscle tone, as well as the pressure transmitted from surrounding structures (26). Moreover, the presence of gravitational forces generates a vertical gradient of P_{pl} in both the upright and supine positions, so that a single value of P_{pl} does not exist. Significant variability in the relationship between P_{pl} and P_{es} is seen with changes from the upright to supine position even in healthy subjects, so that in the latter position higher values of P_{es} are found at each lung volume (27), likely as a consequence of the cranial displacement of the diaphragm and the weight of the mediastinum. Indeed, in either position, P_{es} is believed to correspond to the value of P_{pl} in the middle of the gravitational plane (28,29).

Table 1 Limitations in the use of actual values of esophageal pressure as a surrogate for pleural pressure

Limits
Elastic recoil of the balloon (if overinflated)
Elastic recoil of the esophageal wall
Vertical hydrostatic gradient of lung inflation
Pressure transmitted by the mediastinum
Elastic recoil of the diaphragm
Transmission of intra-abdominal pressure
Presence of inter-regional differences in pleural pressure
Asymmetrical lung disease
Presence of pleural effusion

Following on the observations made by Agostoni *et al.* (30), tidal changes in Pes closely correlate with changes in the Ppl applied to the surface of the lung, then allowing to estimate transpulmonary pressure as the difference between alveolar pressure and Pes (31). Pes is believed to represent the local pressure along its own gravitational plane; then, absolute values of Ppl in other parts of the chest may theoretically be different even for patients with healthy lungs. For these reasons, concerns have been raised for the ability of Pes to track changes in Ppl in the supine position. Moreover, elevation of IAP and changes of lung volume secondary to position may also influence the value of Pes (32). When parenchymal consolidation is present, in addition to the gravitational gradient of Ppl, local variations may also be present, because of the resistance to parenchymal shape deformation (33); such diseased lungs are often inhomogeneous and less deformable, and increased inter-regional differences in Ppl due to shape change may occur (34,35).

Another limitation in the estimate of Ppl from Pes is the presence of an asymmetrically compromised lung (36). In an experimental study, the author found how the effect of unilateral pleural effusion caused different volume-altering effect in the two lungs; yet, the calculated transpulmonary pressure did not seem to be affected by fluid instillation, so that a single local pressure could not be used to assess the stresses acting in different areas of a heterogeneous thorax.

In addition, in patients with ARDS, the dependent lung regions collapse under the weight of the superimposed tissue, and a vertical gradient of lung inflation is established (37); as a consequence, the actual value of

Pes may be different from the Ppl in the most dependent and nondependent lung regions. Seminal experimental studies by Pelosi *et al.* demonstrated how the actual value of Pes provided an accurate estimate of the Ppl only in the mid-lung zone (38); however, respiratory changes in Pes closely mirrored the changes in Ppl across the different gravitational areas even in diseased lungs (38).

In summary, actual values of Pes provide an accurate surrogate of Ppl only in a localized area of the lung, while at the same time overestimating or underestimating it in other regions. In this way, the use of directly measured Pes to calculate transpulmonary pressure and guide mechanical ventilation may avoid lung collapse or promote recruitment only in the area around the esophageal catheter; however, this setting may actually induce derecruitment or overdistention in other parts of lung. Despite the numerous shortcomings presented, the possibility to estimate Ppl at the bedside is regarded as a necessary step towards an approach to lung protective ventilation more tailored at the individual level. Far from being perfect, estimations of transpulmonary pressure are considered of invaluable help to allow the evaluation of the interactions between the ventilator setting, the extent of the disease and the individual patient characteristics, a further step towards the provision of precision medicine in respiratory critical care.

Transpulmonary pressure: different definitions and assumptions

The actual stress exerted on the lung tissue is represented by its transmural pressure, i.e., the difference between alveolar and Ppl (*Figure 1*). Given that during static conditions (as during an inspiratory hold) alveolar and airway opening pressure are the same, the transpulmonary pressure (Pl) is generally estimated as the difference between airway and Ppl. Pl is the pressure that drives the movement of air between the environment and the alveoli, and it may be generated by a negative Ppl as during spontaneous breathing (when inspiratory muscles contract, leading to an increased volume of the chest wall and the generation of a negative pressure), positive as during controlled mechanical ventilation (when the ventilator provides positive pressure at the airway opening) or a combination of the two in assisted modes of breathing.

To avoid the pitfalls associated with the well-known limitations of the use of Pes as a surrogate for Ppl, different models have been proposed to estimate Pl; every method for the estimation of Pl is based on assumptions, and there is

Table 2 Different methods for the computation of transpulmonary pressure

Method	Computation	Assumptions	Reference
Directly measured	$Pl_{ei} = Paw_{ei} - Pes_{ei}$; $Pl_{ee} = Paw_{ee} - Pes_{ee}$	Actual values of Pes reflect actual values of Ppl	(17,39)
Elastance-derived	$Pl_{ei} = Paw_{ei} \times El/Ers$	Pl and $Ppl = 0$ at atmospheric pressure; Elastance should be linear during inflation	(16,19)
Release-derived	$Pl_{ei} = Paw_{ei} - (Pes_{ei} - Pes_{ATM})$; $Pl_{ee} = Paw_{ee} - (Pes_{ee} - Pes_{ATM})$	$Ppl = 0$ at end-expiration and atmospheric pressure	(40)

Pl_{ei} , transpulmonary pressure at end-inspiration; Paw_{ei} , airway pressure at end-inspiration; Pes_{ei} , esophageal pressure at end-inspiration; Ppl , pleural pressure; Pl_{ee} , transpulmonary pressure at end-expiration; Paw_{ee} , airway pressure at end-expiration; Pes_{ee} , esophageal pressure at end-expiration; El , lung elastance; Ers , respiratory system elastance; Pes_{ATM} , esophageal pressure at atmospheric pressure.

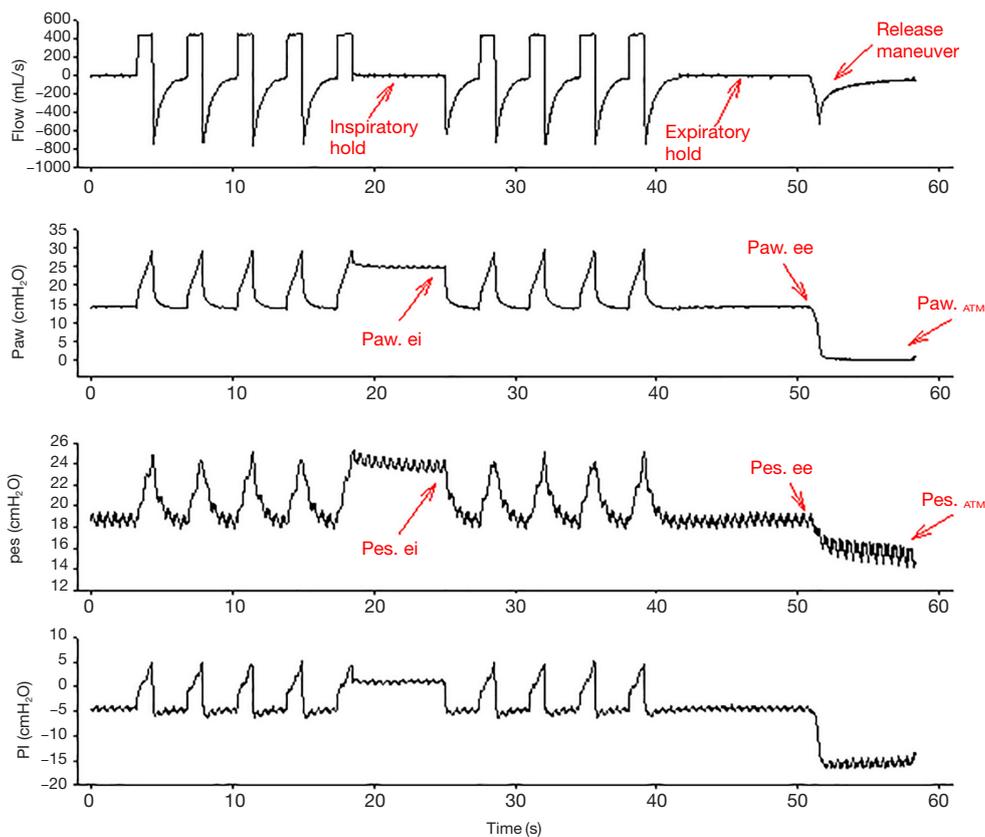


Figure 3 Tracings of flow, airway (Paw), esophageal (Pes) and transpulmonary (Pl) pressure during controlled mechanical ventilation, along with an end-inspiratory and an end-expiratory hold and a release maneuver in a representative patient. Paw_{ei} , airway pressure at end inspiration; Paw_{ee} , airway pressure at end-expiration; Paw_{ATM} , airway pressure at atmospheric pressure; Pes_{ei} , esophageal pressure at end inspiration; Pes_{ee} , esophageal pressure at end-expiration; Pes_{ATM} , esophageal pressure at atmospheric pressure.

no clear evidence of the superiority of any of them. *Table 2* summarizes the different methods, their assumption and the relevant references; *Figure 3* shows representative tracings

of airway and Pes used to calculate transpulmonary pressure with the different methods during controlled mechanical ventilation.

Elastance-derived measurement

In an attempt to remove the confounding influence of the mediastinal weight, assuming that its influence is constant throughout the respiratory cycle, this method, proposed by Gattinoni *et al.* (16), estimates the end-inspiratory PI as the product of plateau pressure times the ratio between lung (El) and respiratory system elastance (Ers). Similarly, end-inspiratory Ppl is plateau pressure times the ratio between E_{cw} and Ers. In other words, this method estimates the portion of P_{aw} that is spent to inflate the lungs only, and the portion that is required to move the chest wall, based on the relative contribution of El and E_{cw} to Ers.

The assumption underlying this method is that, for mathematical reasons, PI and Ppl are 0 at atmospheric pressure: if true pressures are higher or lower than 0 when P_{aw} is 0, the calculated pressures will be under or over-estimated, respectively. Secondly, since elastance is calculated using the tidal change in P_{aw} and Ppl, these variations should be linear during tidal inflation. However, elastance may depend on lung volume, and it may lose its linearity at the extremes of the pressure-volume relationship.

With this method, given that in a system composed by two elastic structures in series:

$$P_{aw} = P_l + P_{pl} \text{ and } E_{rs} = E_l + E_{cw};$$

Then

$$P_l = P_{aw} \times E_l/E_{rs} \text{ and } P_{pl} = P_{aw} \times E_{cw}/E_{rs}.$$

Release-derived measurement

A potential source of bias of the elastance-derived method is that expiratory P_{es} is measured at PEEP rather than atmospheric pressure. The release-derived method estimates PI as the change in P_{aw} and Ppl due to both PEEP and tidal ventilation. PI is then calculated as the difference between P_{aw} and P_{es} from end-inspiration or end-expiration to atmospheric pressure (18):

$$PI = (P_{aw} - P_{aw} \text{ at atmospheric pressure}) - (P_{es} - P_{es} \text{ at atmospheric pressure}).$$

Indeed, at end-expiration at atmospheric pressure, Ppl is equated to zero, whatever the absolute value of P_{es}. This assumption is believed to lead to a lesser bias than assuming Ppl equal to the absolute value of P_{es} (41). In fact, values as high as 10–15 cmH₂O may commonly be found at atmospheric pressure in patients with ARDS, casting doubts as to whether this is compatible at all with an open lung (35,42). In contrast, as seen before, convincing evidence shows how changes in P_{es} reasonably track the

changes in Ppl (21,43,44).

A recent study compared the value of PI obtained by the elastance-derived method with that measured through a “release” maneuver by disconnecting patients from ventilators and allowing them to exhale to atmospheric pressure (40). The authors showed how the elastance-derived end-inspiratory PI was closely correlated with the release-derived value; while it did not require patients to be disconnected from the ventilator, the elastance-derived PI can then be easily used as an estimate for end-inspiratory stress.

Direct measurement

With this method, proposed by Talmor and colleagues (17,39) PI is simply calculated as the absolute difference between airway and P_{es}:

$$PI = P_{aw} - P_{es}.$$

As a consequence of the assumption that actual values of P_{es} reflect absolute values of Ppl, many patients show negative end-expiratory PI. This has been suggested to reflect lung regions at risk of cyclic tidal opening/closing or lung collapse; the negative value of PI is but a mathematical consequence of the calculation method, and it may depend on proximal airway closure during exhalation, alveolar flooding or it may be due to regional variations in Ppl in inhomogeneous lungs. The crude calculation of absolute PI has raised doubts about its reliability, as several confounding may affect the actual value of P_{es}, as extensively stated earlier.

In an attempt to reconcile these conflicting approaches, an experimental study was recently carried out. Yoshida *et al.* measured P_{es} across a range of PEEP levels, together with directly measured Ppl in non-dependent and dependent pleural regions, both in a swine model of lung injury and in human cadavers (45). The authors also computed PI with both the directly-measured and the elastance-derived method, and found how both methods reasonably reflect the “true” PI, although in different lung regions.

Indeed, directly-measured PI tightly mirrored “true” PI in the regions close to the esophageal balloon (i.e., dependent-to-middle lung). Thus, directly-measured end-expiratory P_{es} may potentially be useful to tailor the level of PEEP needed open atelectasis in dependent regions. On the other hand, end-inspiratory PI, as obtained with the elastance-derived method, was found to reflect the “true” local PI in the non-dependent areas. Then, with this method, PI may be used to find the highest level of

inspiratory stress, and it may be used as a target to reduce VILI.

Transpulmonary pressure assessment during controlled mechanical ventilation

Since P_{aw} and tidal volume have proven inadequate surrogates for lung stress and strain (18), the use of PI has been proposed as a better means of adjusting the settings of mechanical ventilation. Despite the sound pathophysiological rationale, clinical studies evaluating the efficacy of such an approach are still lacking. During controlled mechanical ventilation, PI has been used with two different aims: help clinicians to provide a sufficient level of PEEP to avoid derecruitment and atelectrauma, or to provide a better estimate of lung distending pressure, then reducing the risk of VILI. These two approaches have been pursued with two different methods for the estimation of PI, namely the directly-measured method and the elastance-derived method, respectively.

An influential trial by Talmor *et al.* analysed the effect of setting PEEP according to the measurement of end-expiratory PI in patients with ARDS (39). 61 patients were randomized to a standard FiO_2 /PEEP table (46) or a strategy based on PEEP increase until directly-measured end-expiratory PI was within a positive range (0–10 cmH_2O). An average 88 mmHg higher PaO_2/FiO_2 ratio and decreased Ers were found in the Pes-guided group. The level of PEEP in the Pes-guided group was significantly higher than in the control group, with no signs of hemodynamic compromise and an end-inspiratory PI always lower than the limit of 25 cmH_2O . However, in a subsequent study, Chiumello *et al.* found how the setting of PEEP based on such directly-measured approach was not related to thoracic CT-scan lung recruitability, nor with lung weight or the severity of the disease, casting doubts about the assumptions underlying the direct method for PI estimation (47).

On the other hand, Grasso *et al.* evaluated whether monitoring lung distending pressure by the elastance-derived end-inspiratory PI (as opposed to the use of plateau P_{aw}) might allow the clinicians to safely increase the level of PEEP with the aim of improving oxygenation and avoiding the unnecessary use of extracorporeal support in patients with ARDS from H1N1 influenza and refractory hypoxemia (19). Indeed, since P_{aw} may depend upon chest wall mechanics and patient respiratory muscle activity, Grasso and colleagues hypothesized that, in selected

patients with severe ARDS, the end-inspiratory PI could be low enough to allow safe increases of PEEP and lead to improved lung recruitment when a relatively large proportion of P_{aw} was dissipated against a stiff chest wall, despite the presence of a high P_{aw} . The authors set a target end-inspiratory PI of 25 cmH_2O in 14 patients. While 7 patients had end-inspiratory PI >27 cmH_2O , and all underwent ECMO, the other 7 had an average PI of about 16.6 cmH_2O . In this group of patients, an average 4.4 cmH_2O increase of PEEP (from 17.9 to 22.3 cmH_2O) lead to improved oxygenation and prevented the use of extracorporeal support.

Despite both using PI as an estimate of the pressure applied to the lung, the two approaches differ significantly in their assumptions, as we highlighted in the previous section. The approach used by Talmor utilizes directly-measured PI to adjust PEEP in order to keep end-expiratory PI >0 cmH_2O (39). Grasso used the elastance-derived method to target an end-inspiratory PI of 25 cmH_2O (19). Hence, application of both strategies to the same patients may yield different results. Two recent studies directly compared the two methods for PI estimation in the same patients in a cross-over fashion. Gulati *et al.* compared the direct and the elastance-derived method with a target of end-inspiratory PI of 26 cmH_2O . The authors found incompatible results between the two approaches, to the extent that differences in the estimate of Ppl could be as high as 10 cmH_2O for a given patient. Moreover, the optimal levels of PEEP recommended by the two methods were discordant and unrelated, so that the suggested changes in PEEP moved into the opposite direction in up to a third of patients (48). Similarly, Chiumello *et al.* compared the directly-measured end-expiratory PI and that obtained by the release method in 44 patients with ARDS (40). Again, the two values of PI were significantly different and unrelated. Moreover, the value of Pes at atmospheric pressure was not related to the extent of lung consolidation or recruitability as assessed by CT scan, nor to the degree of hypoxemia or the value of chest wall elastance. On the other side, the end-inspiratory PI estimated with either the elastance-derived or the release-derived methods showed a good correlation. In a subsequent study (47), the same authors found how in a cohort of 51 patients with ARDS with different severity of the disease, the PEEP levels suggested from targeting an end-expiratory PI >0 were unrelated to lung recruitability (as assessed by lung CT scan) and similar for all patients despite the severity of their disease.

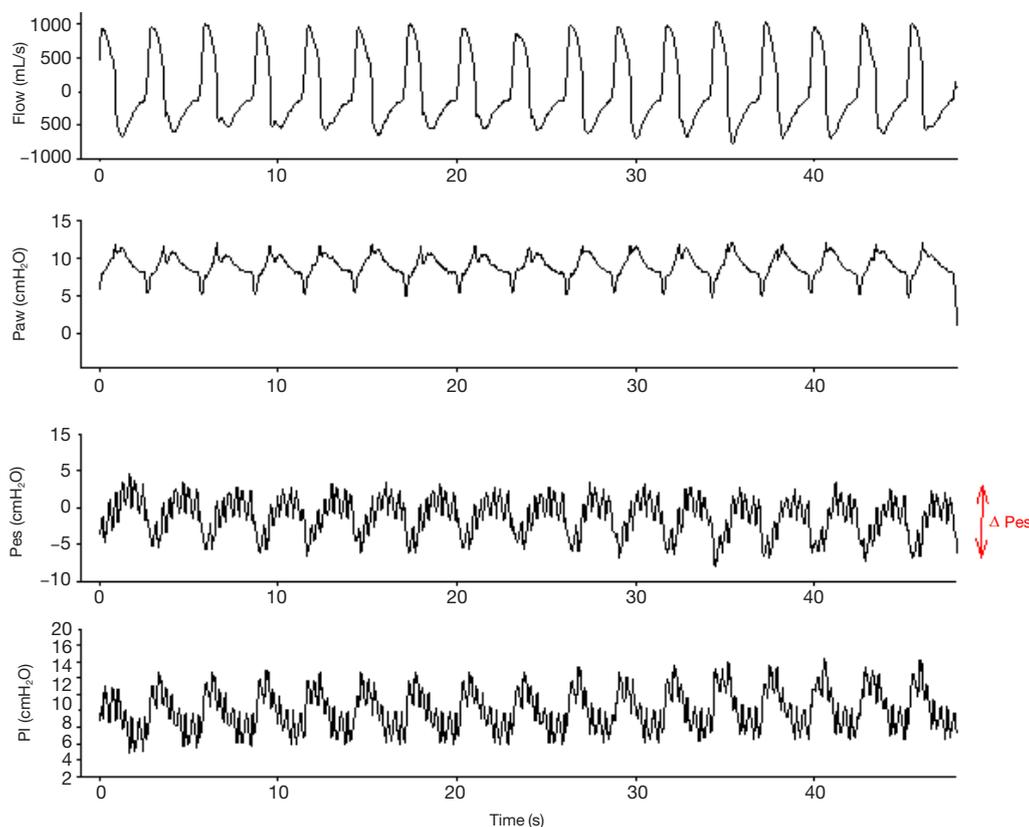


Figure 4 Tracings of flow, airway (P_{aw}), esophageal (P_{es}) and transpulmonary (P_l) pressure during assisted mechanical ventilation in a representative patient. ΔP_{es} , tidal swing in esophageal pressure.

In summary, although clinically feasible, the calculation of P_l from P_{es} as a strategy for tailoring ventilator support at the individual level still needs to be supported by further trials. Since every method for the estimation of P_l is based on assumptions, also the choice of which method to use should be guided by further investigations.

Transpulmonary pressure assessment during spontaneous/assisted breathing

During assisted modes of mechanical ventilation, the total WOB is shared between the mechanical ventilator and patient muscles. Then, according to the equation of motion, the pressure required for lung inflation is the sum of the pressure generated by the respiratory muscles (P_{musc}) and that applied by the ventilator to the airway (P_{aw}). During such a breathing, active contraction of the diaphragm and other inspiratory muscles triggers the mechanical breaths, and the total pressure developed by the muscles depends upon both the respiratory drive and the strength of the

muscles. As a consequence, P_{aw} does not mirror P_l , since the downward displacement of the diaphragm generates a negative P_{pl} swing. Since P_l is the difference between the positive pressure provided by the ventilator, minus the negative pressure generated by the respiratory muscles, P_l is in general even higher than P_{aw} . *Figure 4* shows an example of the contribution of positive P_{aw} and negative P_{es} to the P_l during assisted breathing.

Indeed, in the presence of vigorous spontaneous breathing efforts, high negative P_{pls} are generated, leading to elevated P_l despite normal-appearing P_{aw} (49). Moreover, patient-ventilator interaction may sometimes be difficult to assess when only the standard monitoring of tidal volume and P_{aw} is used. Measurement of P_{es} may allow the clinician to assess patient's real respiratory effort, patient-ventilator (a)synchrony, the presence of intrinsic PEEP and the calculation of patient and ventilator contribution to the total WOB. Assessment of P_{es} may guide the titration of the level of ventilator support at the individual level, as well as to monitor the level of fatigue

during a weaning trial and even to predict the failure of the weaning process. Monitoring P_{es} allows to calculate the pressure-time product of P_{es} , an index related to the metabolic cost of breathing; during a trial of spontaneous breathing, this index significantly increased only in patients who then failed weaning (50). The tidal swing in P_{es} , used as an index respiratory effort, was shown to progressively increase as patients failed a weaning trial (51), and it allowed better discrimination between patients who failed and those who succeeded the trial than conventional index such as the rapid shallow breathing index (52).

Recently, Bellani *et al.* conducted a study aiming at comparing the tidal change in transpulmonary pressure during assisted breathing and controlled ventilation, after matching for similar conditions of airflow and volume, in a group of patients undergoing different levels of pressure support ventilation followed by a phase of controlled mechanical ventilation (12). The authors demonstrated how, for a given flow and tidal volume (assuming unchanged mechanical properties of the system), tidal changes of P_l were similar between the different conditions of support and regardless of the level of inspiratory effort, whereas the absolute value of airway and P_{es} were different, thus highlighting the importance of measurement of P_{es} during assisted modes of breathing. In fact, preservation of spontaneous breathing was shown to be associated with different beneficial effects, such as improved hemodynamics (53), a better ventilation-to-perfusion matching (54), and a reduced extent of muscle atrophy (55). However, other studies found how spontaneous breathing efforts could potentially worsen lung injury (49,56,57), likely because of the effects of negative intrathoracic pressure (which may lead to interstitial edema), generation of unsafe stress and excessively elevated P_l and loss of control over tidal volume. In an experimental model of ARDS, allowing spontaneous breathing had beneficial effects in terms of lung recruitment only in case of mild lung injury, whereas it worsened lung injury in more severely ill animals, likely because of the development of injuriously high transpulmonary pressure (57). In this regard, even if no studies have so far been conducted in patients, end-inspiratory P_l should likely be kept $<20-25$ cmH₂O, which is the upper limit of physiological range (20).

In summary, monitoring P_{es} during assisted modes of ventilation is highly relevant. First, estimation of P_l may prove invaluable to detect the harm of spontaneous efforts; second, it may allow individual titration of ventilator

support to prevent diaphragm injury and accelerate liberation from ventilation.

Conclusions

Despite data showing its relevance, assessment of P_l and P_{es} monitoring is still hardly used in critical care medicine. This may partially be due to technical issues, such as proper placement of the esophageal catheter, and because of the difficult interpretation of the measurements. However, a strong pathophysiological rationale, and an increasing amount of clinical evidence convincingly show how this technique may provide an invaluable insight for the management of critically ill patients, both during controlled mechanical ventilation (to allow partitioning between lung and chest wall) and during assisted ventilation (to assess the contribution of respiratory muscles and the interaction with the ventilator).

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Footnote

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